V_0



Space Engineering

STRAIN ACTUATED AEROELASTIC CONTROL

Kenneth B Lazarus

January 23, 1992

Project Sponsors:

NASA Langley Research Center General Dynamics Corporation

National Science Foundation

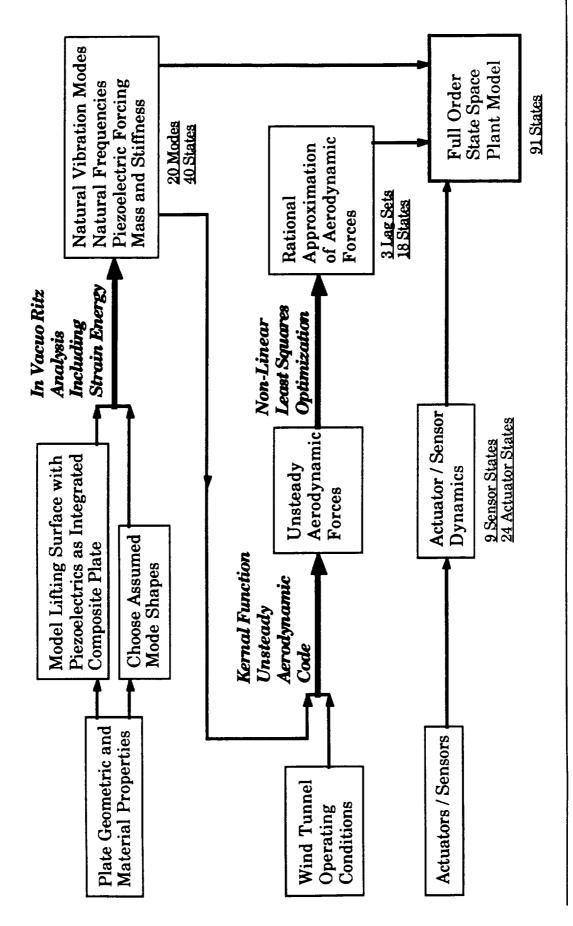
PROJECT GOAL

- Develop and Demonstrate Strain Actuated Lifting Surface Technology for Aeroelastic Control
- Induced Strain Actuation, rather than conventional articulated methods, allows for:
- Control of the Lifting Surface Shape for Altering the Aerodynamic Forces
- Direct Control of the Strain in the Structure and Dynamic Mode Shapes

SPECIFIC OBJECTIVES

- Develop a Capability for Analyzing Plate-Like Aeroelastic Lifting Surfaces
- Develop MIMO Control Laws for the Strain Actuated Adaptive Wing
- Demonstrate that Strain Actuation is an Effective means of Achieving Aeroelastic Control

STRUCTURAL AND AERODYNAMIC MODELLING



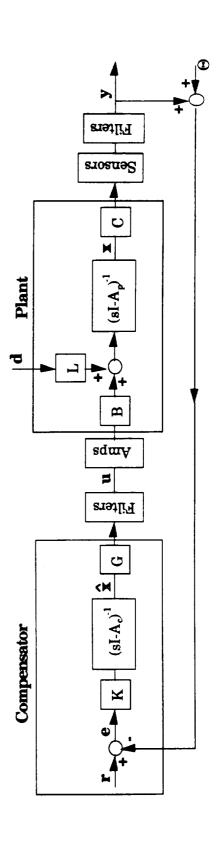
Space Engineering Research Center

CONTROL LAW DESIGN METHODOLOGY

- Reduce "Full" Order Model to 'Design" Model
- Obtain Minimum Realization
- Find Hankel Singular Values
- Retain Modes with Largest Hankel SVs and DC Components of Others
- Design Linear Quadratic Gaussian Compensator
- Cost Minimization
- Loop Shaping
- Reduce 'Design' Model to 'Controller' Model
- Same Procedure as Above
- Optimal Projection

SYSTEM BLOCK DIAGRAM

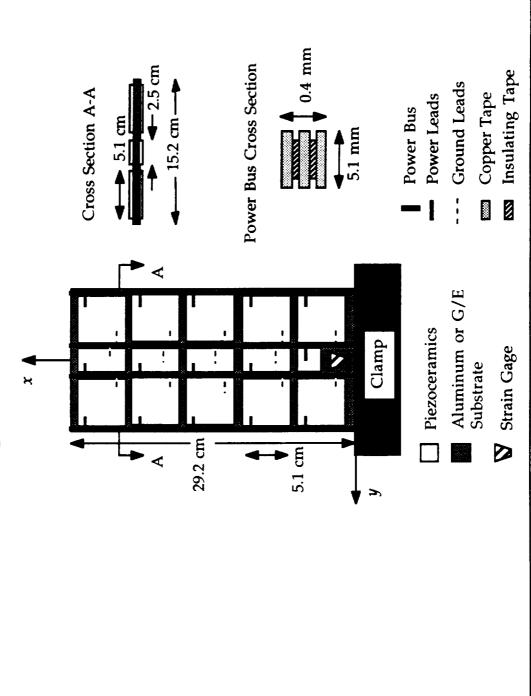
- Plant Model from Raleigh-Ritz and Unsteady Aerodynamic Analysis
- Sensor, Amplifier and Filter Dynamics Included in "Full" System
- Magnetic Shaker (Bench) or Gust Generator (WT) Disturbance Source
- MIMO Compensators Designed using Reduced Order LQG or Optimal **Projection Theory**
- Compensators Implemented by a Real Time Digital Control Computer



Space Engineering Research Center

ADAPTIVE WING TEST ARTICLE

Cantilever Plate Configuration: Actuators Cover 71% of Plate



Space Engineering Research Center

BENCH - TOP EXPERIMENTS

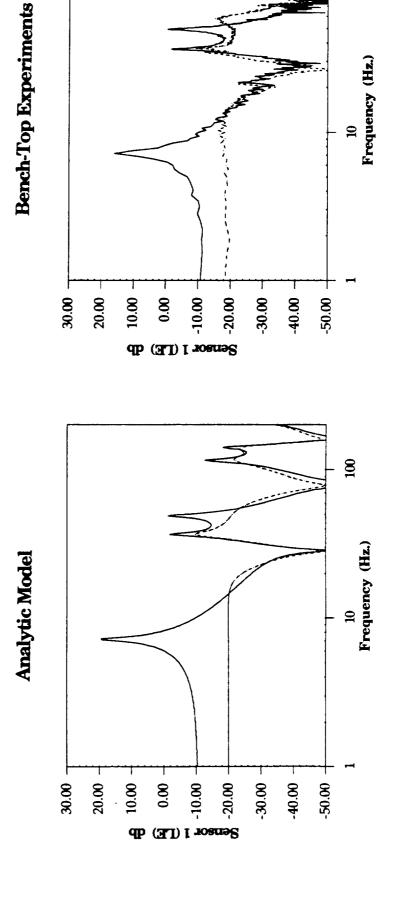
- Correlate Analytic Model and Check Hardware Functionality
- Verify Control Law Design Procedure and Gain Necessary Controller Design Experience
- Demonstrate High-Authority Large-Bandwidth Disturbance Rejection Capabilities

100

BENCH-TOP DISTURBANCE REJECTION: OPEN AND CLOSED LOOP RESPONSE

- Aluminum Bench Mark Specimen
- Reduced Order LQG Design: $\rho = 1e^{-2}$

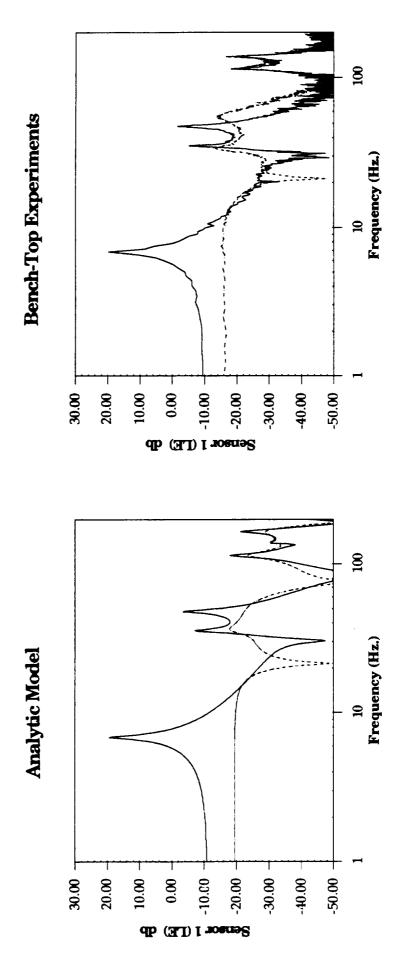
Sensor Noise = 3.0%



BENCH-TOP DISTURBANCE REJECTION: OPEN AND CLOSED LOOP RESPONSE

- Graphite/Epoxy Bend/Twist Coupled Specimen
- $\rho = 1e^{-2}$ Reduced Order LQG Design:

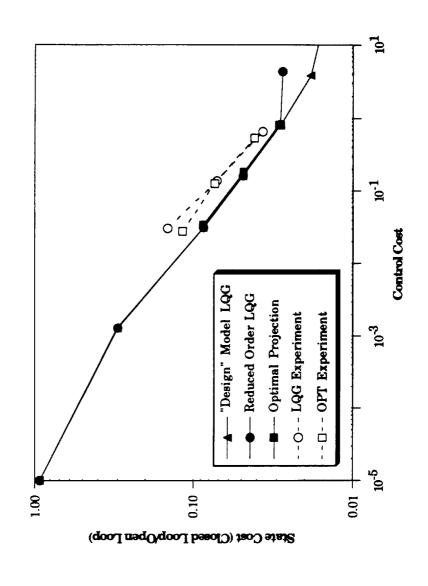
-2 Sensor Noise = 3.0%



BENCH-TOP DISTURBANCE REJECTION: STATE COST VERSUS CONTROL COST

- Aluminum Bench Mark Specimen
- Reduced Order LQG & OPT Designs:

Sensor Noise = 3.0%



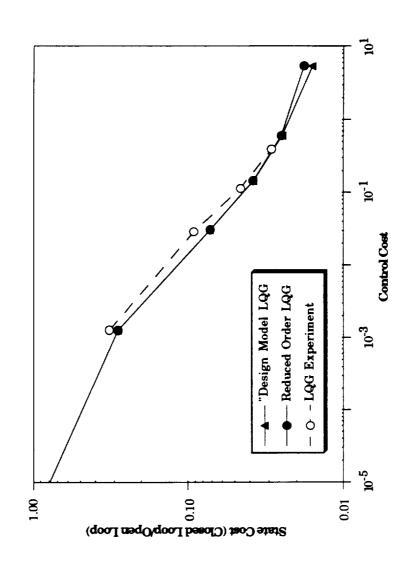
State Cost Reduced by 96% (14 db RMS)

BENCH-TOP DISTURBANCE REJECTION: STATE COST VERSUS CONTROL COST

Graphite/Epoxy Bend/Twist Coupled Specimen

Reduced Order LQG Design:

Sensor Noise = 3.0%



State Cost Reduced by 96% (14 db RMS)

WIND TUNNEL EXPERIMENTS

Aeroelastic Control Issues

Performance Objectives

Flutter Suppression

Vibration Suppression

Gust Alleviation

Maneuverability

Control Law Objectives

Stability

Plant Regulation

Disturbance Rejection

Low Frequency Command Following

Result: A Well Regulated Plant with High Loop Gain in the Low Frequency Regime is Desired

WIND TUNNEL SET-UP

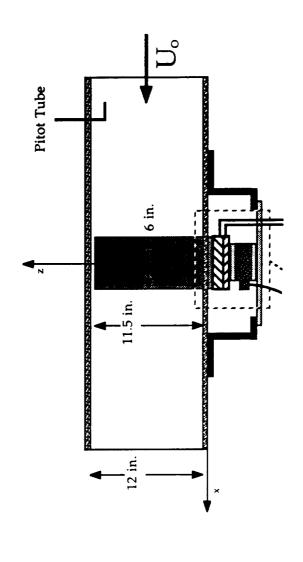
1 Foot Low Turbulence Tunnel

- Test Section: 8" x 12"

- Maximum Speed: 100 MPH

Gust Generator 1 Semi-Chord Ahead of Leading Edge

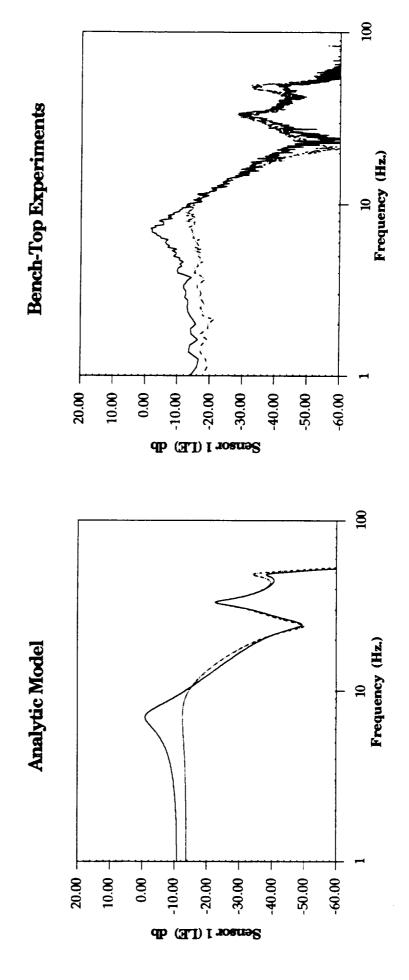
Laser Displacement Sensors Built Into Side of Test Section



OPEN AND CLOSED LOOP RESPONSE AT 60 MPH WIND TUNNEL GUST ALLEVIATION:

- Aluminum Bench Mark Specimen
- Reduced Order LQG Design: $\rho = 1e^{-1}$

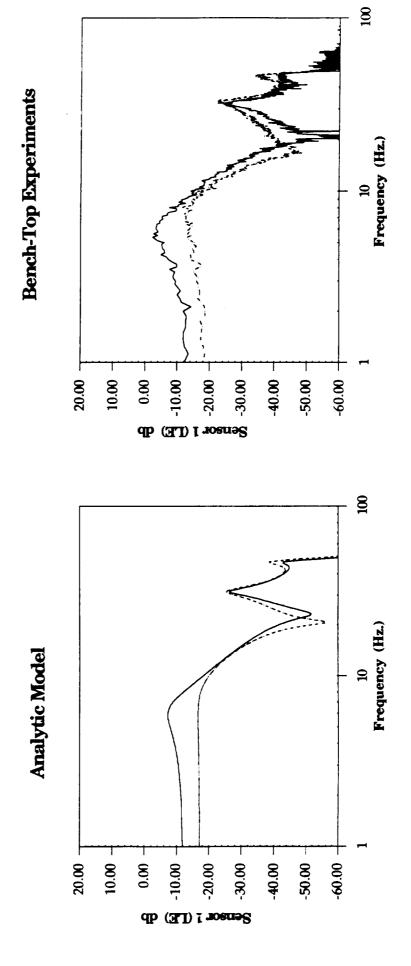
Sensor Noise = 1.0%



WIND TUNNEL GUST ALLEVIATION: OPEN AND CLOSED LOOP RESPONSE AT 60 MPH

- Graphite/Epoxy Bend/Twist Coupled Specimen
- Reduced Order LQG Design: $\rho = 1e^{+0}$

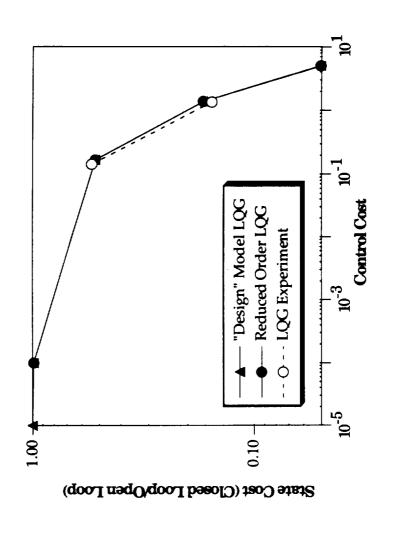
Sensor Noise = 0.5%



WIND TUNNEL GUST ALLEVIATION: STATE COST VERSUS CONTROL COST AT 60 MPH

- Aluminum Bench Mark Specimen
- Reduced Order LQG Design:

Sensor Noise = 0.5%

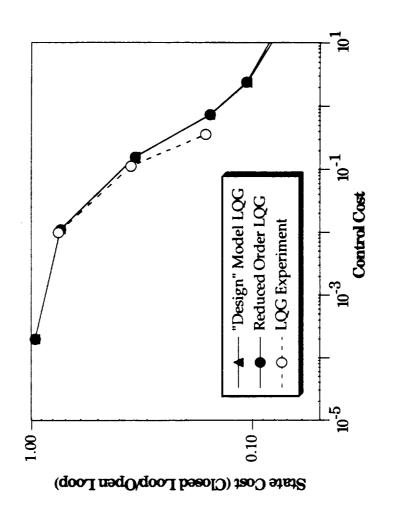


State Cost Reduced by 84% (8 db RMS)

STATE COST VERSUS CONTROL COST AT 60 MPH WIND TUNNEL GUST ALLEVIATION:

- Graphite/Epoxy Bend/Twist Coupled Specimen
- Reduced Order LQG Design:

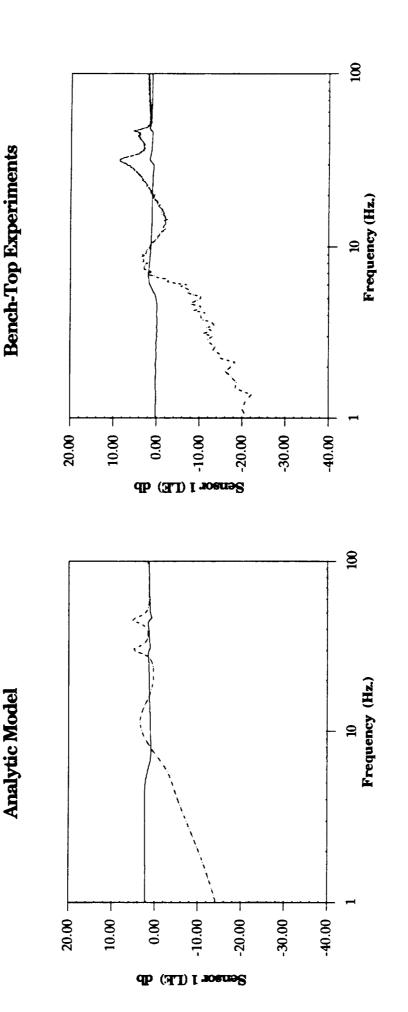
Sensor Noise = 1.0%



State Cost Reduced by 84% (8 db RMS)

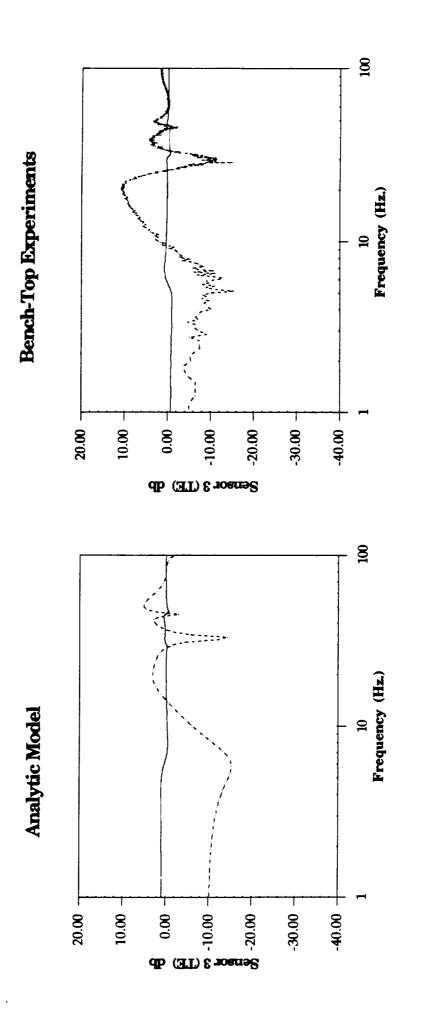
OPEN AND CLOSED LOOP ERROR AT 60 MPH WIND TUNNEL COMMAND FOLLOWING:

Low Bandwidth Graphite/Epoxy Bend/Twist Coupled Specimen:



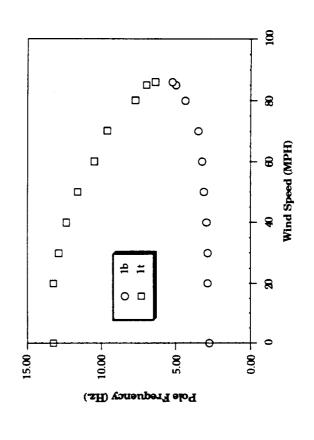
OPEN AND CLOSED LOOP ERROR AT 60 MPH WIND TUNNEL COMMAND FOLLOWING:

High Bandwidth Graphite/Epoxy Bend/Twist Coupled Specimen:



WIND TUNNEL FLUTTER SUPPRESSION: OPEN LOOP FLUTTER SPEED

- Aluminum Plate Original Flutter Speed About 125 MPH
- Flutter Speed Lowered to 88 MPH by:
- Adding 1.6x Original Weight
- 0.8 Semi-Chords Behind the TE



WIND TUNNEL FLUTTER SUPPRESSION: CLOSED LOOP STATE COST CURVES

- Finite State Cost (stable system) for Any Control Weight
- High Frequency Modes Are Destabilized as Gain Becomes Large

